

A Review Paper on Specimens Size and Shape Effects on the Concrete Properties

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Abstract

Concrete properties are the most essential and critical physical material property when reinforced concrete structures are planned. Because of the development and in types and nature of material used to enhance the concrete innovation, materials and mix proportions, test measure, mixing strategy, and testing condition have noteworthy impacts on highlights of concrete strength, in light of the fact that the control specimen sizes and shapes might be unique in relation from State to State. Testing of mechanical properties (especially compressive strength and tensile strength) of concrete is one of the most urgent stages of development. To control the nature of the concrete, there are different molds used for pouring concrete samples according to different directions in different countries. Many researchers have realized that the specific shapes and sizes of concrete samples can cause different types in the consequences of compressive strength or tensile strength. The relationship between the compressive strength of the concrete cube and the cylinder is complex. The cylinder and concrete cube samples were compared in the pressure test by studying previous research, including the test methodology, factors affecting the cylinder / cube strength ratio, and the coefficients, equations and components of the conversion factors. Previous attempts to determine experimental transformational relationships and conversion factors have proved that it is disturbing (if not impossible) to predict the relationships between the forces of the cylinder and the cube. Previous research has shown that the ratio of the strength of the cylinder / cube is between 0.65 and 0.90, despite the fact that the ratios outside this range have been found similarly. In light of this review of previous research, the test of the cylinder is not initiated by testing the cube. This study is a review of the sample size and shape effect on concrete properties.

Keywords: Concrete properties, compressive strength, size effect, shape effect, Specimen size.

Introduction

Concrete is the second most used material on the planet. It has many valuable properties including strength, durability, accessibility and economy. For any development construction, the compression resistance test sample should be used. It is difficult to determine which type of mold, cylinder or cube, even better in countries where cubes are standard molds, there is in all calculations inclined, anyway for investigation purposes, to use cylinders instead of cubes, of test research facilities. For most countries, the sizes and shapes of the test molds to determine the compressive strength of the concrete are unique. In any case, normally utilized molds are usually cylinders and cubes.

The cylinders (150 * 300 mm) are used in the United States, South Korea, France, Canada, Australia and various countries although the cube (150 mm) is standard molds used in the UK, Germany and many other European countries figure 1. There are a few states (for example, Norway uses 150 * 300 mm cylinder and 150 cubic mm), where tests are performed on two molds. The cylinders are accepted to give more interesting consistency to the results of the molds, which can be compared in the light of the fact that their failure is less affected by the restriction of the molds in the end. Their strength is less affected by the rough aggregate properties used in the concrete mixture. and the stress dispersion on flat planes in a cylinder is more uniform than on cube shape [1,2].

It should also be remembered that the similar concrete mixture will not give compressive strength that cannot be distinguished when tested from cubes and cylinders. The force of the estimated pressure on the cubes is consistently higher than that of the cylinders [3]. It can be seen that the cylinders are constructed and inspected similarly, while in a cube molds it cast at the line of activity of the loads at right edges to the pivot of the block as-cast.

In the primary compression section, the circumference of such a current is in a test cylinder and has been recommended. Therefore, the tests on the cylinders are more practical. The communication between the directions formed and tested, however, has shown no significant effect on the strength of the cubes made of Heterogeneous and heterogeneous mixture. The size of the test templates is supported to test the force in important standards, but all of this is often allowed over one size.

In addition, both now and then have advanced convictions to use small templates. These bring their points of interest, the smaller molds are less demanding to deal with, they are less inclined to damage, the molds are less expensive, the machine needs less testing limits, less concrete is used, which means less lab capacity and less space, and more Much smaller amount of preparation [4].

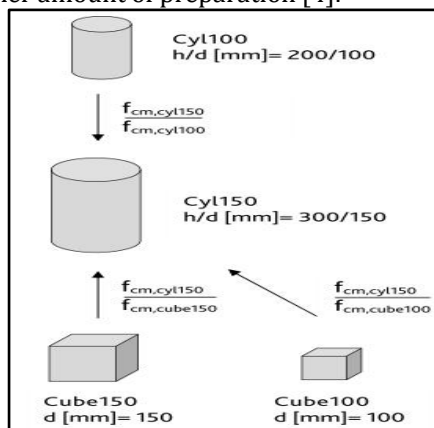


Fig. 1 Standard Shapes of the molds used in many countries

It is not expected here to recapture the debate about the gains and negative aspects of the concrete test, either as cube shapes or cylinders. When testing the superior concrete as a shovel, the parallel between the two faces of the two acid tests appears to be a basic test.

The lack of parallelism can increase the number of shear times, which tend to reduce the strength of compressive strength. Therefore, to re-establish the parallel between the two cubes, from the basic either use composite under the surface or to crush, the use

of cube molds does not take care of the issue of final arrangement, similarly, individuals working with the two shapes know well the burden of utilizing the cube shape, for cleaning, careful support is required and be prohibitive when contrasting and molded forms of plastic cylindrical shaped molds [5].

The standard molds for compressive strength testing for concrete are cylinder (150 * 300mm). If the ratio of h / d is equal to (2), if the concrete mixture is tested in pressure using a variable scale cylindrical mold, when the diameter is extended to 457.2mm, a significantly smaller reduction in stress is examined. Such diversity in stress with a variety of measurements and molds is relied upon by the expansion of realistic homogeneity in concrete molds. The more obvious the geometry of the templates can affect the research test information on the strength of the concrete.

The strength of the cylinder mold with (L / D) on (2) or the measurement above (304.8mm) is only slightly affected by the effects of volume [1]. It has been discovered that the control effect of the test machine's cylinders extends throughout the cube, but is not affected by a piece of test drum. In this way, it is not natural for the strengths of the cubes and the resulting cylinders to vary by a similar mixture of concrete [2]. As shown by changing the strength of the cylinder to the strength of the equivalent cubes in BS 1881: Part 120, the cylinder strength is equal to (0.8) of the strength of the cube so far, as a general rule, there is no basic connection between the strength of molds of two shapes.

The ratio of the strength of the cylinder to the cube increases unambiguously with the expansion of the force and is almost (1) in force more than (100MPa). Some of the different components were also found, for example, the moisture condition of the molds in the test hours to influence the strengths of the qualities of two types of molds. Since the European standard (ENV 206: 1990) recognizes the use of the two cylinders and cubes, it includes a proportional scale for the strength of two types of compressed molds up to 50 MPa. (Estimated on the basis of cylinders).

The ratio of the cylinder / cube ratio is close (0.8). CEB-FIP Design Code gives a comparative table for comparison. In any case, more than 50 MPa, the strength of the cylinder / cube increases dynamically and 0.89 at the power of the cylinder (80MPa). Neither of these tables should be used for motives behind the deliberate conversion of power from one type of mold to another of a force.

The issue is to know exactly what it got the compressive strength (100Mpa) on (150 * 300mm).

Such communication is reported for common concrete. For example, [Carrasquillo P.M. And Carrasquillo R.L., 1988] found that (150 * 300mm) gave (7%) compressive strength higher than (100 * 200mm) to (48 to 80MPa). [Morino J., 1990] In fact, expansion (1%) was found in compressive strength when it was estimated at (100 * 200 mm) instead on (150 * 300 mm). [Cook J.E., 1989] proved that for a concrete strength (70MPa), (100 * 200mm) had a higher compressive force (approximately 5%) than 150 * 300 mm.

It has been revealed in principle that pregnancy failure increases with the decline of this ratio and that efforts to reach a "standard" estimate turn out to be highly confusing because of the varying level of strength of concrete pressure as well [6]. There are certain specifications, to ensure the strength of axial compression, taking into account the large variation in (aspect ratio) regardless of whether it is more prominent than (2). The range ($5 > b / h > 1$) of the aspect ratio has been recommended, taking into account the avoidance of torsion and the unequal final distribution of the pressure distribution. For the most part, three types of failure were observed in the solid concrete form under the pressure of unidirectional pressure: pyramidal or conical shape, axial shape and oblique single level.

ASTM C 42-90, AASHTO T 22 and BS1881: Part 120: 1983 refer to the presence of stress factors for concrete forces, as shown in Table (1). Conversion factors are given in the AASHTO and ASTM codes to evaluate the strength test results at ($h / d < 1.8$). These elements convert the strength test results to equal results for a mold containing ($h / d = 2$).

Table 1: Cylinders Strength with different ratios of h/d and Standard correction factors

(h/D) ratio	correction factor of strength	
	ASTM C42-90/AASHTO T22	BS 1881. Part120
2.0	1.0	1.0
1.75	0.98	0.97
1.5	0.96	0.92
1.25	0.93	0.87
1.0	0.87	0.8

For the most part, these factors are used to perform tests on centers taken from structures, where the ratio ($h / d = 2$) cannot always be obtained for examples, the general relationship between h / d and power is shown in Figure 2. It is clear from the figure that the force ratio is closer to 1.5 ($h / d > 1.5$).

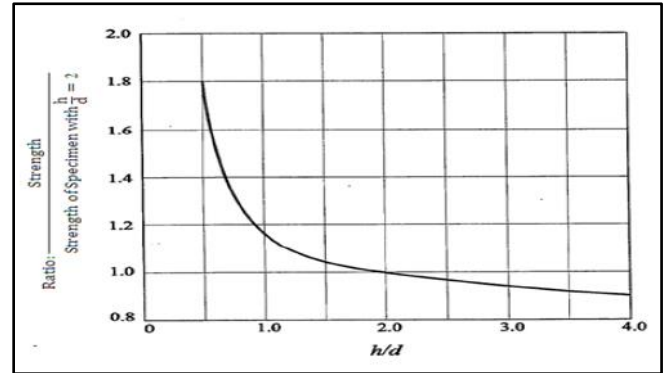


Fig. 2: Relationship between (h/d) ratio and strength ratio

Compressive strength of concrete can be resolved utilizing distinctive states of specimens. Most ordinarily utilized specimens are cylinders and cubes. The cubes shapes are littler contrasted from the cylinder, and the benefits of cubes don't rely upon the the quality and condition of molds and their density can be done quickly and accurately by weighing and estimating. Impact of shape of the molds on the compressive strength of concrete has been generally considered and distinctive connections have been proposed between the cylinder and cube compressive strength.

According to Indian Standards (150mm) cubes are utilized for deciding the compressive strength of concrete. Utilization of (100 mm) cube has its favorable circumstances. The (100mm) cubes are simpler to deal with and will bring about sparing of materials, relieving space, stockpiling and work.

The general investment funds can be noteworthy in money related terms. In any case, designers and modelers are hesitant in utilizing (100mm) cubes for deciding the compressive strength due to the apparent more prominent changeability in their compressive quality over that of the (150mm) cubes. Additionally, there is an absence of consistence criteria for the (100mm) cubes as the General Specification gives acknowledgment criteria in light of (150mm) cubes strength as it were.

In the mid-1980s, large-scale compressive failure was considered; the effect of size on the strength of quasibrittle material that collapses after a major development in the stable crack is most likely to occur through the release of energy. Inquiries about the effect of pressure on loading have turned into a focal point of enthusiasm among specialists.

[J. K. Kim and Y. Seong, 2002] investigated the effect of the ratio of the ratio to the height on the compressive force, while accepting that the estimation of the regression point shown in Figure 3 was roughly selected as 45 because the friction effect

by the friction force would be immaterial if It turned out that the aspect ratio (h / d) was large. Accordingly, the cylinder with $h / d = 1$ will have the ability to resist higher loads than the cylinder ($h / d = 2$).

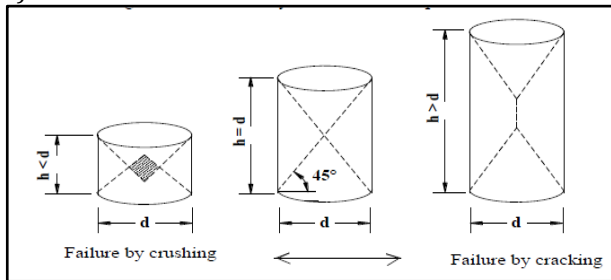


Fig. 3: Specimen geometry failure modes

Why compressive strength of concrete cube is more noteworthy than that of cylinder.

Purposes behind cube to have more noteworthy compressive strength when contrasted with cylinder are as appeared in figure (4):

- contact region of a standard cube with the upper platen in the compression machine is more which results in greater restriction.
- more control opposes against mold extension bringing about more compressive strength.
- The proportion through cube and cylinder strength is regularly thought to be but not constant (1.25).

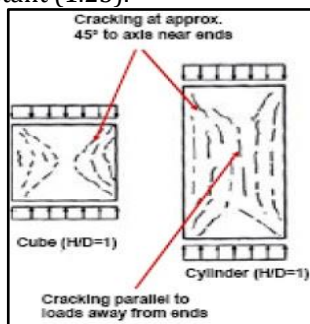


Fig. 4: Cube and cylinder mechanism of failure comparison

The different variables incorporating characteristic varieties in concrete quality and correlation among cylinder and cube strength influences the strength ratio:

- **Effects of cube/ cylinder casting, curing and testing techniques**

The technique for casting and topping of cube and cylinder influences the strength proportions of both. The utilization of unbending and non-inflexible molds influences their strength. Additionally, the strategy for topping these molds influences the strength as out of plane surface likewise impacts their

strength proportion. Appropriate curing and testing method is important to relate a legitimate connection between cube and cylinder compressive strength proportions, generally the proportion got will deceive.

- **Effects of geometry of molds**

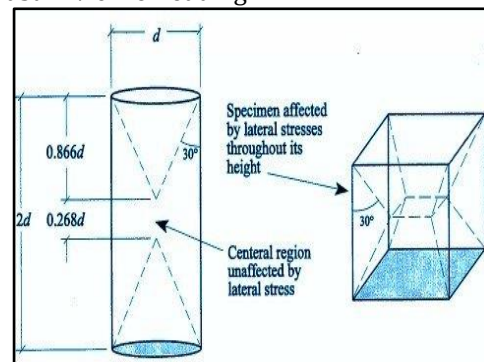
Geometric factors, molds shape, volume of concrete, and h/d proportion of molds influences the cube and cylinder strength proportion. Figure (5) demonstrates the impact of (h/d) proportion to the strength of the concrete proportion.

- **Effect of strength of concrete**

The strength of mixture has been appeared to influence the cube and cylinder strength proportion. Research demonstrates that this proportion diminishes with expanding concrete strength. Cylinder to cube strength proportion ranges from (0.77 to 0.96) contingent upon concrete strength level.

- **Loading direction and machine qualities**

cubes might be loaded toward the path opposite to throwing while cylinders are constantly loaded toward throwing. Since cubes and cylinders are built in numerous layers, their strength will contrast in view of loading



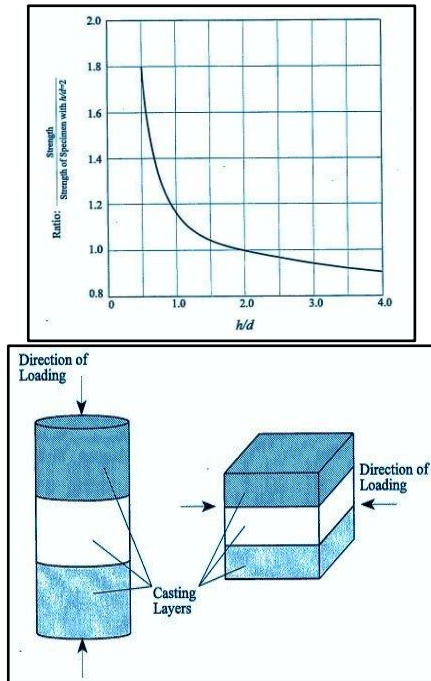


Fig. 5 Effect of (height h./diameter d.) ratio to strength ratio of concrete.

• **Aggregates Grading**

It influences the strength of any structure. The impact of compression test on concrete mold are substantial because of relative size of total particles to mold measurements. Most measures sets restraint for the proportion of diameter or size of molds to greatest ostensible size of aggregates. Normally, this admissible least is near (3 to 4).

The cylinder (d = 150mm and h = 300mm) is a standard for testing pressure strength in the United States. While in Britain and Europe, the standard example of the pressure quality test is the cube scale (150 * 150 * 150 mm). Cubes are smaller than cylinders. The advantages of cylinders do not depend on the quality and condition of the molds, and their density can be faster and more accurate in terms of weight and estimation. The basic distinction between the shape of the cylinder and the cube is that the cylinder requires placing it above it before loading in light of the fact that the best surface of the cylinder that was wrapped by the shovel does not cause any level of testing.

Two strategies are used to get the plane surface of the cylinder. (I) bridging strategy. (II) Milling technique. The cubes do not require a top where they are loaded. The ratio of h / d is equal to (2), the pressure of the cylinder with oscillating diameter, the larger the diameter, the lower the force. The cylinders are

constructed and tested similarly, but the cubes are poured in one way and tested at the right edges of the position, so no cover or cracking is needed.

In the original structures in this area, the loading and selection processes are similar to those in the cylinder and you do not like the cube. Comparing the strength of the pressure between the cube and the cylinder is 0.8, which is often associated with the natural strength of the force.

Figure (6) shows the effect of the compressive pressure ratio expected to estimate the slope, selected almost as (45 °) because the effect of friction to prison will not be relevant if the angle angle (h / d) rotates to be wide. In this way, the cylinder with the perspective ratio (h / d = 1) will have the ability to resist high loads more than the cylinder by angle (2). The typical fracture of the cylinder is the cone and there are different types of cylinder cracks as shown in Figure (7) (ASTM C 39). Figure (7.b) illustrates the typical failures of the cube (Neville and Brooks, 2010; BS EN 12390-3, 2002).

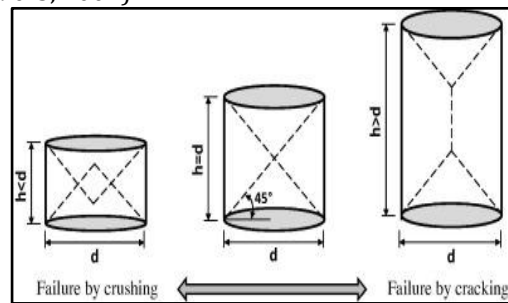


Fig.6: Effect of the specimen size and failure modes

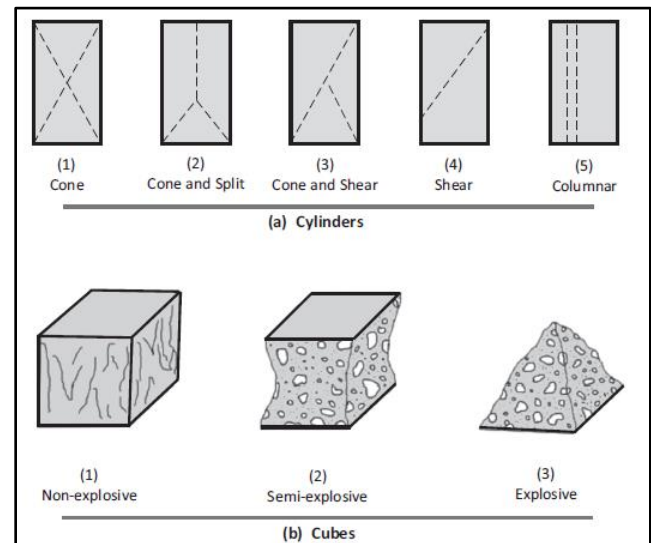


Fig. 7 (a): Fracture types sketches of cylinders (ASTM C 39). (b) Typical cube failure mode (BS EN 12390-3, 2002).

Literature review

[Jin-Keun Kim, et.al., 2000] estimates the estimated final strength of a flexural member, the influence of a member's size is not usually considered. For different types of loading, however, power is reliably reduced as the size of the members expands. In this examination, the effect of the volume of the flexing part was examined by tests. For this reason, the development of c-shaped examples of axial load bearing and twisting moment was experienced using three unique sizes of concrete blocks with a pressure strength of 52 MPa.

The three examples of the outstanding size were in the position and width of their intersecting regions, where the ratio was 1: 2: 4. The thickness of the molds was consistent, taking into account the effect of size in the external planning cycle. The test results are combined with at least a square strategy (LSM) for the new parameters of the MSEL.

The (MSEL) curve, which has been charted with new parameters, and the unidirectional pressure strength of the concrete drum test results are compared; the results show a more significant measurement effect in the C-cast segment compared to the cylindrical individuals. The pressure tests were completed for 21 models of C-shaped concrete and the cylinder, molded from a similar group with a pressure of 52 MPa, to assess the effect of the compression on the flexure strength and strain and the bending pressure of the flexural.

The effect of measurement is clear, ie, the compressive pressure at failure decreases with the estimated increase in estimation. Recommended new MSEL parameter estimates that better predict low power. The impact estimate for compressive pressure in the C model examples is even more important for the single-axis compressor pressure. Similarly, the effect of size on the strain is assessed by the final bending (bending and elasticity) and the relationship between stress and tension. The volume effect can be connected to pressure by MSEL, as well as compressive pressure.

[Song Tai Yi, et al. Al., 2006] In this study, the effect of sizes, shapes and headings on the compression of molds was examined in principle in the light of fracture mechanics. First mode tests were performed using the cylinder, cube and sawdust. The test results of the installation curve use less square strategy (LSM) to acquire the new parameters of modified volume effect law (MSEL). The results of the investigation show that the effect of mold sizes, shapes and final strength is available.

Similarly, contacts are examined between pressure, size, shape and mold placement. All materials have

special physical characteristics. For each material, the properties are viewed as unique when they are independent in size and shape. For standard purposes, standard drum pressure (150 * 300 mm) is recognized as a basic and vital material. In any case, the basic idea is that concrete pressure is a great physical property that is incorrect since compression changes in light of sizes and shapes, for example because of crack properties.

They concluded that the effect of cube size and filters was more affected than cylinders. For compression, the equations applied to cylinders, cubes and filters are suggested. Furthermore, to obtain cylinder pressure from other cast shapes, suitable models are suggested regularly for each of the mold templates.

For the effect of position on the piston, the NSC cubes do not appear to have a clear effect. For HSC, if possible, the distinction is obvious. For NSC saws, when the title of the case is parallel to the loading direction, the pressure is lower than normal. For the HSC, be it as it may, the opposite end was discovered.

The effect of force on the effect of the shape decreases with increasing mold size. More specifically, for HSC, the mixing of pressure between the strengths and cubes fades more rapidly than the NSC difference. The findings suggest that existing quality standards based on the guidelines for practice should be reformed. When designing solid structures, the most attractive to utilize the compression is not from the institutional molds, for example, cylinders (150 * 300mm) or (100 * 200mm) so far of the molds in light size, shape and the main position of the real structures.

[Benjamin G. also, Marshall D., 2008] A test program was directed to determine whether interchangeable template templates could be used reliably to determine UHPFRC in the range of 80 to 200 MPa. Precise guarantee of high-strength concrete pressure is now an alarming recommendation because of the requirements of reducing the requirements of extensive testing machine and cylinder preparation requirements. Fifty-one, 76, and 102 mm cylinder were tested close to the molds 51, 70.7, and 100 mm cube. It has been observed that 76 mm cubes in addition to the 70.7 and 102 mm cubes are good options in contrast to the standard molds with a diameter of 102 mm. 70.7 mm cubes are proposed for conditions where the order of the machine or the arrangement of the potential cylinders is a concern.

[J.R. Del Vizo, et al. al., 2008] The objective of the exploratory program was to consider the effect of size and shape on the pressure tests conducted on the HSC, in search of the effect of shape and measurement of molds on HSC pressure. In the mechanical procedure of the HSC (about 100 MPa) try in the

compressed setting in the axial pressure control and propose another connection between the cylinder molds and cubes and they have investigated the variety types in the crack pattern and in the mechanical behavior due to the size and condition of the molds. The cylinders and cubes of different sizes as shown in Figure 4 are used to perform stress strain tests. The tests were performed in a single axial stress rate.

This estimate remained constant throughout the testing program. The results show that the post-peak behavior of the cubes is less severe than the behavior of the cylinders, resulting in the use of strong energy after the end. This is reliable with crack pattern perception: the small fission rate through the molds is denser in the cubes than the cylinders. In fact, a basic slant surface is encased in cylinders, although there are cubes where we get the parallel limbs and there is a thick vertical split in most of the molds. Explore the compression relationship given by two types of templates to a few templates. We hypothesized that pre-shock and postpeak behavior in stress strain curves are subject to the size and shape of the mold.

The cubes reveal a mild failure state on the contrary, with limitations on the hardness of the cylinders. Test results indicate the size of the effect. Larger molds resist less stress than small ones. The impact of the cubes is more affected by the cylinders, where the natural force is generally fixed within the temporary size that is ready for the exploration. See the crack pattern after careful testing of the molds situation.

The surface of an initial slant is moved in a cylinder, although in the cube they find that the horizontal wrap around it and that there is a deep vertical split in the weight of the molds. This is predictable with observed differences in stress and strain curves between cubes and cylinders. Significantly, the failure design does not change with size. The size of the model shows the compression of cubes in a basic model in the light of fracture mechanics ideas.

The connection between the standard cylinder and the strength of the cubes of any size is determined. It detects the effect of measuring cubes and can derive the relationships between the pressure of cylinders and cubes, within the scheme of decomposing fractions.

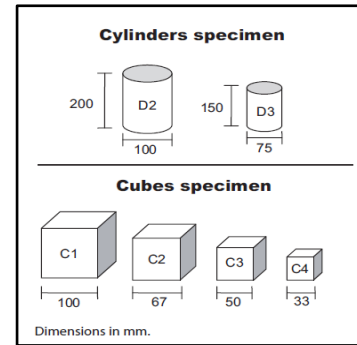


Fig. 8 specimen geometry with different shapes

[NiloufarZabihi, 2012] This examination focused on the effect of mold molds and shapes on the pressure and hardness of the concrete, was restored in different conditions and tried in all the early and late ages. Density was performed in the hard case, non-destructive tests (ie, hammers and PUNDIT), and compressive tensile strength divided into different treatment cases. A few tests were carried out to obtain the components of change and the relationship between these variables and the results. Examination results show that for all test conditions, there is a strong impact for a variety of size and condition of the molds. Again and again, by changing treatment conditions, the difference in the pattern of exploratory results was not significant, for example, PUNDIT test results.

However, by changing the age of the test, there was a strong adjustment in the results and patterns. The effect of the distinctive mold size and shape effect on the effects of non-harmful tests was taken along with the destructive experience of pressure and pressure. Through investigations, shift factors have been converted to change the pressure or tensile strength of the different molds to each other, and tried to see how these elements change by changing the processing structure, the age test and the outline mixture. The total exploratory area of this assay included various probes, for example, VeBe time, stagnation, concrete density in hardened state, ultrasonic velocity, hammer test, compressive force and tensile strength.

He found, by diminishing the w/c proportion, the concrete workability of mixture diminishes. Changing mixture outline, and decreasing the w/c proportion, density of concrete in hardened state of molds increments due to having more grounded bonds. High strength concrete can cause interruptions in the expanding pattern. Types of curing causes the normal density changes. Density of molds is bringing down for the ones aired cured. As the cubic molds measure size maximize, the molds brought about higher ultrasonic speed. The perceptions can be because of

more grounded (more homogeneous) bonds and higher most extreme total density in bigger molds. Portion of coarse increments, if the max aggregate measure is kept consistent, littler solid mold may result in higher ultrasonic velocities than greatest molds (cube=200 mm).

The results of PUNDIT tests are less dispersed in larger templates that show more homogeneous patterns. Hammer test results against pressure tests are directly real for the GGBS mix. The results of the hammer test for the larger molds were considered smaller than the small molds. Because there is a very identical set, the test is more careful to stroke on the coarse aggregate of cement. The effect of authorship therapy can also be seen in the results of the hammer test. Treatment in water makes tests on the surface more texture. In this way, the treatment of water molds has higher results in the hammer test. Therefore, treated water samples have higher hammer results. If we consider tensile strength of all forms of molds, the regression in the tensile vs. compression graph has a wide pattern. The development of the tensile pattern through pressure on different shapes is unusual.

The cubic shapes show the shapes strongly increment while the cylinders have a gentle expansionist pattern. Tensile of solid molds has the tendency to have a variable pattern by changing the estimate of the templates. Up to a certain width, continuously by expanding the size of the molds, and tensile damping. After a certain point, the tensile starts to increase. The effect of the size and condition of the molds on tensile strength is more pronounced in higher strength. The compression results were unambiguously influenced by the sizes of their samples and their effect on the wall. When the mix links are weaker, the pressure results are more consistent, as the compression of molds is controlled by bond strength. The sample sampling times (for different sizes and shapes) are equivalent and, if ordered as a direct or high grade concrete, the transformational variables of many templates will have comparative patterns.

In order to test the molds to control the quality of the mixing work, it seems (150 x 300 mm cylinder) the most reliable examples. By reducing the proportion of the parallel surface / volume of the molds, the pressure increases. At the point where the molds reach 28 days, the natural change factor of the treated water pressure and treated in the air molds is equivalent to or slightly different. After a specific purpose of the pressure curves, the cylinders are characterized by a sharp decrease pattern while the style cubes are more moderate. Cubic templates contain a higher contrasting cylinder.

Patterns of fracture of templates of different shapes in addition to the unusual. The discs contain a basic break surface that causes sharp cracking. The cubes have a fractured surface that gradually develops and gives shape to the glass design. Stress and strain curve arrangements are in line with mold breaking models. Cylinders unload a lot of energy suddenly (sharp reduction), while the cube forms energy discharge step by step. In all concrete mix schemes by amplifying the size of examples, the area under load deformation reduces the increases because the molds can retain more energy until broken.

[E. I. Al-Sahawneh, 2013] Reducing the pressure of natural weight molds, particularly with extended h / b quota, is a matter of serious concern. This paper explains the shear slippage model with an illustration of the implementation of the degree of 1.0 of the quality treatment factor at h / b 2.0 2.0. The theoretical test was performed on the proposed model using shear planes to select the sliding planes.

A general case is proposed to anticipate correction factors taking into account the effect of h / b and pressure pressures. The templates have been with different variables under load pressure. The proposed model for failure of the shear with an indicative study of the ratio of the aspect ratio of the force to the strength of the final compression of the molds at different edge ranges and the selection of the quality review factor. It is clear that the model thinks of looking at the reasons for the impact of the insignificant size of the concrete and can deal with a larger set of issues.

[FarhadAslani, (2013)] This paper talks about a trial program that was completed to ponder the impacts of example size and shape on the compressive and rigidity of SCC and fiber RSCC. Alterations in the blend plan of SCC may essentially impact the material's mechanical properties. In this manner, it is essential to examine whether all the expected speculations about regular cement additionally remain constant for SCC structures. For this reason, cube shape molds with (100 and 150 mm) and cylinder molds with (100*200 and 150*300 mm) were built. The trial program analyzed four SCC mixture: plain SCC, and steel, polypropylene and half and half fiber RSCC. Compressive and elastic were tried after 3, 7, 14, 28 and 56 days.

The paper additionally researches connections among's compressive and tensile and the size and state of the molds. The trial program comprised of 30 molds with cube shape with (100 and 150 mm), and 30 cylinder molds with (100* 200 and 150*300 mm). Additionally, it inspected four SCC blends plain SCC, and steel, polypropylene and half and half fiber RSCC.

Compressive and tensile were tried after 3, 7, 14, 28 and 56 days.

He presumed that, measure impact in view of the molds size and shape contrast is available for SCC and FRSCC mixture. The impact of size on cube is more noteworthy than that on cylinder for all the inspected SCC mixture blends. The DS-SCC mixture has a higher compressive than alternate blends in all molds. Moreover, the D-SCC mixture has a higher elasticity than alternate mixture for (100*200 mm) and (150*300 mm) cylinder.

To acquire the solid compressive and rigidities, the connections of the size impact for cube molds and for cylinder were recommended in view of break mechanics. Besides, these connections are relevant to N-SCC, D-SCC, S-SCC and DS-SCC. The proposed relationship of the size impact for cubes and for compressive and tractable cylinder starts with a similar standard. Be that as it may, in strengthened SCC mixture, the compressive and splitting conditions are extraordinary; this marvel is identified with the compressive and splitting of N-SCC and the fiber reinforced record.

The introduced test results demonstrate the presence of a shape impact. Shape impact investigations demonstrate that the cube shape's quality is lower or almost equivalent to the strength of the cylinder for D-SCC mixture for all measurements. Besides, these examinations showed that the shape's strength is higher or almost indistinguishable to the strength of the cylinder for N-SCC, S-SCC and DS-SCC for all measurements. The proposed connections are useable for FRSCC and ordinary SCC. Notwithstanding, the primary parameter that ought to be adjusted in light of the new mixture configuration, by aligning this parameter the introduced connections and results in this examination are helpful for variable SCC examinations.

[M.A.S. Sudin and M. Ramli, 2014] A lightweight mixture, such as foam, is an adaptable material consisting mainly of bond-based mortar mixed with at least 20% of air volume. Its dry density is regularly below 1600 kg / m³ with a maximum pressure of 15MPa. The standard ASTM order determines a concrete treatment agent somewhere in the range (14 and 42 MPa), with a specific final target to set a lower force, where h / d is an example below (2.0).

If so, the order of CEB-FIP specifically determines the quality of the cylinder (150 * 300mm) to 150mm of the cube; however, both the preconditioning of the precursors does not specifically cover the material, the weight. The pivotal point in this work is to think about the effect of example size and shape on the

compression of the mixture. Molds of various sizes and shapes are thrown with square and round intersections, ie cubes, prisms and cylinder. Their compression practices were discussed in 7 and 28 days. The results show that, as shown in the order of CEB-FIP, regardless of ornamental concrete, the shapes (100mm) ($l / d = 1.0$) offer equivalent compressed quality with a cylinder (100 * 200mm) ($l / d = 2.0$).

Three different combinations were prepared, including the use of (a) alternative forms of molds (eg cubes, prisms and drum), with l / d 1.0 and 2.0; (b) the same templates by estimating the different shapes; and (c) cube molds with different sizes and shapes; So, with ($l / d = 1.0$). It illustrates a case in order using various shapes and sizes. The effect of size and shape (ie, area shape and aspect ratio) of the mold was examined on foam mixture compression at a unit weight of 1250kg / m³.

The cylinder template showed a slight change in pressure when the l / d value changed from 1.0 to 2.0. Contrasts with cube mold. The truth is told, the f_{cu} of the extended cylinder as l / d is extended; whereas for the cube, there was a 18.2% decrease in pressure. The steel shape can convey a higher load than the cylinder (cross sections remain unclassified). In the ratio and shape of the similar l / d (cube), the compressive quality of the foam concrete, did not decrease f_{cu} with the breadth of the mold size. For the foamed concrete, the 100mm steel shape ($l / d = 1.0$) creates an equivalent equivalent decompressor and $d = 100\text{mm} * h = 200\text{mm}$ cylinder ($l / d = 2.0$).

[Abd, M. K. Furthermore, Habib, Z. D. 2014] The assay is expected to demonstrate the effect of size and shape on self-compressive compressive pressure (SCC). The work is isolated into two parts. The first is the regular concrete (NC), high strength concrete (HSC) and self-chewing concrete (SCC) between 25-70 MPa. from locally accessible materials. The cylinder to cube strength were between (0.86-0.9) of NC, (0.94-0.96) of HSC and (0.96-0.99) of SCC. The second is to explore the impact of size on compressive, the estimations of correction factor of (150*150*150 mm) and (100*100*100 mm) cubes are (0.89-1.29) of NC, (0.98-1.26) of HSC and (0.98-1.22) of SCC. The estimations of cylinder adjustment factor of (150*300 mm) and (100*200 mm) is (0.88-1.08) of NC, (0.93-1.07) of HSC and (0.95-1.04) of SCC. The impact of shape was diminishing when the compressive expanding. The compressive of cylinder or cube with measurements littler than standard is higher strength of the bigger molds. Revision factor of SCC for cylinder and cubes scopes to one. Suggested of utilizing any shape or size of molds when SCC create

with a better characteristic on condition of fresh and hardened.

[Ritu Kumari, 2015] This paper examines the relationship between compression of cubes shapes and cylinders for different evaluation processes of the mix. Standard size cube shapes (150 x 150 x 150 mm) were restored and tested after 7 days and 28 days each. Standard size cylinders (d = 150mm and h = 300mm) are restored and tested after 7 and 28 days each. From testing the previous test information, the standard cube and cylinder were tested for 7 days and 28 days. The result shows that the strength of the cube is more worthwhile than the standard cylinder power.

In the testing of cube shape, the molds are influenced by parallel stresses all through its length. On account of cylinder standard, the focal area is unaffected by parallel stresses. The locale of $0.866d$ from the highest point of the cylinder and the distance of $0.866d$ from the base of the cylinder is influenced by parallel stresses and the focal area of $0.268d$ is unaffected by sidelong stresses.

As indicated by the impact of platen limitation on the method of failure is more noteworthy in a cube shape than in a standard cylinder, the strength of cube shape is around 1.25 times the strength of cylinder, however the genuine connection between the strength of two sorts of shapes relies upon the level of strength and the dampness state of mixture at the time of testing. It is sensible to ask whether a cube shape or a cylinder is a superior test example. cylinder is less end restriction and a more uniform dissemination of stress over the cross segment, hence the cylinder quality is most likely closer to the genuine uniaxial compressive strength of mixture than the strength of the cube.

As per the IS-516-1979 indicated that the cube strength of controlled molds will be not the same as the standard cylinder strength. Ordinarily cylinder strength is taken as 0.8 times the cube shape strength, however exploratory consequences of past research so that there is no novel connection between the cube and the strength of cylinder shape. As indicated by every trial datum of the connection among cylinder and cubes, expressed that the strength of cylinder is certifiably not a consistent estimation of 0.8 times the strength of the cube since it relies on such a large number of elements like w/c proportion, coarse aggregate (reviewing, surface, shape, quality and firmness) and the most extreme aggregate size, concrete substance and the day and age.

[Raj Kumar, et., al., 2015] The mixture utilized in dams and different structures may change in character contingent upon the utilization of fixings

and site conditions. All cements produce warm as the cementitious materials hydrate. The vast majority of this warmth age happens in the main days after arrangement. For thin solid segments, for example, asphalts, heat scatters nearly as fast as it is produced. For thicker solid areas (mass solid), heat scatters more gradually than it are created. The net outcome is that mass cement can get hot.

Administration of these temperatures is important to counteract harm, limit deferrals, and meet undertaking determinations. The best method to decrease the temperature ascent of mass cement is to lessen the generation of heat. This can be accomplished by utilizing concrete of low generation or potentially by diminishing the bond content. In such manner, the one financially savvy strategy is the decision of the biggest conceivable size of coarse aggregate.

For a given weight, higher the most extreme size of aggregate, bring down is the surface area of aggregate and the other way around. As the surface territory diminishes, the water request additionally reductions to coat the particles and create usefulness. Bigger most extreme size of aggregate requires lesser fine total substance to keep up cohesiveness of mixture blend. As a result of its lower water request, favorable position of higher most extreme size of aggregate can be taken to bring down the concrete utilization. For quality control amid development, planning of check examples for deciding compressive is fundamental.

This prerequisite if there should be an occurrence of mass solid utilizing expansive size coarse totals is hard to meet due to the absence of lab and testing hardware to deal with substantial examples. Along these lines, extraordinary measures must be considered from which the "wet-screening" technique is the most generally utilized one. To decide the connection of compressive between the extensive size cube molds and size solid shapes, cube with 45cm were thrown utilizing genuine solid blend which incorporates vast aggregate and cube=15 cm size were set up from wet screened mixture blend.

[Betar Matulić, et al. al., 2016] Study effect of the test effect on the mechanical properties of the sprayed cell. The tested concrete lab test was filmed in an emotionally supporting core network in the paper. The effect of the sprayed concrete model scale on the compressive and dynamic coefficient of elasticity of normal cement and fibers reinforced by fibers delivered at the site is dissected.

The outcomes are utilized to examinations reasonableness of assessing compressive in view of the dynamic modulus results. The examination of results demonstrates that the compressive proportion

of plain shotcrete tests 50 mm and 100 mm in high, without the expansion of fiber, adds up to 1.20, while this proportion in fiber mixture adds up to 1.26.

The outcomes affirm the connections of compressive tests with the size proportion of 1:1, and the examples with the base measurement to tallness proportion of 1:2, as characterized in principles HRN EN 13791:2007 and HRN EN 206-1:2006. The molds with fiber and superplasticizers result in a more prominent homogeneity, thus the got compressive qualities indicate less dissemination. The coefficient of variety is bringing down in smaller sample tests, which focuses to a higher probability of experiencing neighborhood abandons in greater molds. Not at all like compressive, the molds with $h = 50$ mm, i.e. the molds with the base distance across to highest proportion of 1:1, have a roughly 10 % bring down modulus contrasted with the molds $h = 100$ and 150 mm, having around a similar powerful modulus.

In this manner, the adjustment in test measure influences the change in compressive and dynamic modulus in an unexpected way. The outcomes acquired affirm the proposal for the base mold height of 100 mm for molds, and this examination built up that this limitation in test tallness likewise applies for concrete with a littler greatest grain estimate. The coefficient of variety of the dynamic modulus is bring down in tests containing fiber and superplasticizers.

Tests have affirmed that a specific relationship exists between the compressive and dynamic modulus results for shotcrete tests $h = 5$ and 10 cm, and equations acquired by connection investigation for surveying the compressive in light of the dynamic modulus results. Be that as it may, while evaluating the compressive quality in light of dynamic modulus results got by means of an ultrasonic gadget, one ought to know about the vulnerability of the technique, since a little blunder in estimating the dynamic modulus causes a critical mistake in the appraisal of the compressive of shotcrete.

The subsequent association may apply to the solid utilized in the essential supportive system of the passage tunnels, while for different kinds of mixture it might fill in as an unpleasant gauge as it were. It ought to likewise be noticed that the tests were performed on water immersed tests, thus certain deviations may happen in the utilization of the association between the compressive and dynamic modulus on some dry molds.

[Misba Gul, 2016] In this paper the impact of the cube shape mold size on the compressive of mixture has been researched. Cube mold of two unique sizes (100 mm and 150 mm) were utilized for throwing of mixture. The pressure tests were performed on all the

cube mold utilizing Compression Testing Machine. The mixture extent was kept the same in every one of the mixture mold during casting. Pressure tests were directed at (7, 14 and 28 days) with (100 mm and 150 mm) cube mold. At last, the impact of shape of mold measure from the compressive of mixture was resolved.

The test outcomes demonstrate that the compressive of cube = 100 mm was higher than that of cube = 150 mm tests. In this trial contemplate the impact of shape estimate on the compressive of mixture has been examined with the goal that a relationship can be produced between the compressive of cube = 100 mm and cube = 150 mm.

The variety in estimations of concrete compressive when testing is done on two unique sizes of (cube 100 mm and 150 mm) territories between (5 to 6 %) the strength got on littler cube shape size being higher. In the event that cube = 100 mm are tried for assurance of compressive of mixture, the acquired strength ought to be lessened by around (5 to 6 %) to accomplish the real strength characteristic.

[Yi Che, et.al., 2016] This paper exhibits the consequence of exploratory examination on splitting tensile strength of self-compacting (SCC) concrete. Splitting Brazilian tests on a progression of SCC cylindrical shaped examples of various $D = 70, 100, 150, 195$ and 300 mm, and of various $H = 75, 100, 150, 200$ and 300 mm, were directed.

Every one of the examples were thrown from a similar mixture with a normal compressive of 61.4 MPa. The aggregate extreme total size was 15 mm. The pressed wood bearing strips with the width to the cylinder shaped distance across proportions, $t/D = 6.7\%$ and 16.7% , were utilized in the tests. The impact of measurement and stature of the examples and in addition width of the bearing strips on the tensile splitting strength were examined. Cracking commencement and spread were likewise checked amid the tests by utilizing strain gages and camera.

Test outcome demonstrates that the splitting of mixture was influenced by the measurement as well as the stature of these examples. For cylinder with same t/D proportion and stature, the strength diminishes as the wide increments, while for the cylinder with same width, the tensile may diminish as the height increments. The strength of SCC molds showed huge size impact, it was influenced by the mold wide, as well as by the shape height. For the molds with a similar size, more extensive load bearing strip may prompt higher strength of tensile.

[K. Ejiogu, et, al., 2017] 170 molds of different shapes and sizes of M30 review of solid molds was delivered which included (100 mm, 150 mm and 200 mm cube

shape, (100 mm and 150 mm) diameter across cylinder and (100 mm, 150 mm based prisms). The compressive test for different shapes created were tried to assess the shapes and measurements that gave the most noteworthy strength of compressive. The cube of (100 mm and 150 mm) with a thinness proportion of one (1) ($h/d=1$) gave the most elevated compressive.

The compressive for the (100 mm) cube at 28 days fix was 41.52 Mpa, and the compressive for the (150 mm) cube at 28 days fix was 39.00 MPa. The compressive quality of the cylinder and cubes diminished as the ratio of slenderness proportion expanded because of the decreased compressive power because of the lessened shear at the platen interface as a steady load was connected by the pressure testing machine.

[Gustavo H. N., et. Al, 2017] This work presents a relative examination of the effect of mold shape and size on compressive quality and flexible mortar coefficient. The mortar is mixed with compression quality somewhere in the range of 5 and 20 MPa.

Test decided the compressive quality of cylinder molds of (50*100mm) and (100*200mm) and furthermore cubic examples came about of mortar's flexural quality tests, which utilize (40*40*160mm) prism. The cylinder molds were likewise decided. Cubic examples' compressive quality was higher than (100*200mm) cylindrical compressive quality and lower than (50*100mm) compressive of cylindrical. The measurements of the cylindrical molds impacted its compressive quality, which was higher for the (50*100mm) molds. Nonetheless, it didn't influence the static modulus of the material.

Results relationships were developed and tests were conducted with different results from the creators, leading to both creative control and cement / lime mortar augmentation.

The cube molds were pressed higher than the cylinder pressure (100 * 200mm) on the form of molds and less than the compression cylinder mold (50 * 100mm). The cylinder mold measurements greatly influenced their compression, which was greater for measurements of measurements (50 * 100mm), but did not affect the constant coefficient of the material. In light of the enormous discrepancy in the results that can be reached in writing on this subject, the current work has added to the mechanical control of concrete lime mortar, examining the effect of different shapes and sizes of molds in ensuring elasticity and compressibility coefficient, and those written by various writers.

[Ali J. H. 2017] This work examines the current effect of volume and shape on HPLWFC pressure with

fiberglass. The foam agent was used for lightweight. Glass fiber size sections were used: (0, 0.06, 0.2, 0.4, 0.6%) by adding a larger amount of mixture. HPLWFC properties were evaluated using new flow and density tests. In this test, the size and size of the molds used for compressing were measured cubes (150 mm cube), (cube=100) and (cube=50mm) and (cylinder =300 * 150mm) and (cylinder =200 * 100mm).

The completion of the HPLWFC mixture revealed the development of compressibility of all mold dimensions with (GF=glass fiber) content. The common size of the molds gave a greater pressure in the variety of distinct dimensions. The difference in compression for two dimensions and shapes has abated with the progress in the GF measurement range. The small measurement of the molds for cubes or cylinders satisfies high pressure to high-density lightweight foam concrete dimensions and sizes. The 50 mm compression inhibitor was prolonged to the S3 mix by 38%, 15% mixed, and 150 mm and 100 mm cubes (S1 and S2).

The normal pressure of HPLFC (cylinders =300*150 mm) to (cube=150 mm) was (0.88). The normal pressure of HPLFC (cylinders =100 * 200mm) to (cube=150mm) was 1.01. The normal ratio of HPLFC (cylinder=150 * 300 mm) to (cube=100mm) was (0.8). The normal proportion of compressible HPLFC (cylinders=100 * 200mm) to (cubic=100mm) was (0.91). The normal division of compressible HPLFC (cylinders=100 * 200 mm) to (cylinder=300 * 150 mm) was (1.15). The normal quotient of compressible HPLFC (cube =100 mm) to (cube=150 mm) cubes was (1.1). The deviation in pressure is reduced from two dimensions and shapes with a rise in the GF size part.

Conclusion

1. This research represents a review on specimen's size and shape effects on the concrete properties
2. The testing specimen and molds differs from country to country in size and shape.
 1. Cylinders, prisms and cubes are available and used in different sizes and shapes.
 2. There are different codes for molds that are utilized for casting concrete samples.
 3. Numerous shapes (h, d) and sizes (50, 100, 150 and 300mm) of concrete moldscan cause varieties in concrete properties.
 4. 4. Standard molds are cylinders and cubes. The cylinders (150 * 300 mm) are utilized in the States, South Korea, France, Canada, Australia and numerousland although the

cube (150 mm) is the gauge molds utilized in the UK, Germany and considerable other European land.

5. The concrete grade effect on concrete properties.
6. The relation between compressive strength of Mixture cube and cylinder is complex.
7. Compression resistance test is performed either using the cube or cylinder. The various standard symbols recommend using a concrete cylinder or concrete cube as a standard sample.
8. For normal concrete the cylinder gives strength lower than cubes.
9. For high strength concrete the difference between cube and cylinder are smaller. That means there are no differences between cylinder and cube (shape and size) for high grade concrete.
10. It should be recognized that comparable concrete will not provide compressive strength that cannot be recognized when examined with cubes and cylinders. The compressive force evaluated on cubes is consistently greater than that achieved on cylinders.

References

1. Neville A.M., Properties of Concrete, Pitman, Wiley, New York and Longman, London, 5th and final edition (2000).
2. Al-Hayderi H.S., Correlation Between Strength of Different Sizes, Shapes and Curing Conditions for High Strength Concrete, M.Sc. Thesis, Al-Mustansiriya University, Baghdad, Iraq, (2003).
3. Mohammed Kareem Abd and Zuhair Dhaher Habeeb, Effect of specimen size and shape on compressive strength of self-compacting concrete, Diyala Journal of Engineering Sciences, 2014, ISSN 1999-8716, 7:02, pp. 16-29, Technical Institute-Babylon, Iraq.
4. K. Ejiogu; P.A.P. Mamza; D.I. Onyemachi; D.I. Brown; N. Adegboro; U. Ibeneme and B.F. Julius, The Effect of the Dimensions of Concrete Samples on the Physio- Mechanical Properties of Normal Concrete Blocks, International Journal of Innovative Scientific & Engineering Technologies Research, (2017) 5:1, pp. 34-43, SEAH PUBLICATIONS.
5. Issa S. A. and Islam M. S. and Issa M. A. and Yousif A. A. and Issa M. A. Specimen and Aggregate Size Effect on Concrete Compressive Strength, Cement, Concrete, and Aggregates, (2000), 22:2, pp. 103-115.
6. Mansur M. A., Islam. M. M., Interpretation of Concrete Strength for Nonstandard Specimens, Journal of Materials in Civil Engineering, (2002), 14:2, pp.151-155.
7. Jin-keum Kim, and Seong-Tae Y., Application of size effect to compressive strength of concrete members, India, (2002), 27:4, pp. 467-484.
8. Morino J., 225W. Wacker Drive, Concrete International: Design and Construction, (1990), 12:1, pp.9-35.
9. Carrasquillo P.M. and Carrasquillo R.L., Evaluation of the use of Current Concrete Particle in the production of High-Strength Concrete, ACI Material Journal, (1988), 85:1, pp. 49-54.
10. Cook J.E., 10000 psi Concrete, Concrete International, (1989), 11:10, pp.67-75.
11. Jin-Keun Kim, Seong-Tae Yi, and Eun-Ik Yang, Size Effect on Flexural Compressive Strength of Concrete Specimens", ACI STRUCTURAL JOURNAL, (2000), 97:2, pp. 291-296
12. Seong-Tae Yi, Eun-Ik Yang, Joong-Cheol Choi, Effect of specimen sizes, specimen shapes, and placement directions on compressive strength of concrete, Nuclear Engineering and Design, (2006), 115-127/2005 Elsevier B.V.
13. Benjamin Graybeal and Marshall Davis, Cylinder or Cube: Strength Testing of 80 to 200 MPa (11.6 to 29 ksi) Ultra-High-Performance Fiber-Reinforced Concrete, ACI Materials Journal, (2008), 603-609. Title no. 105-M68.
14. J.R. del Viso, J.R. Carmona and G. Ruiz, Size and Shape Effects on the Compressive Strength of High Strength Concrete, Cement and Concrete Research, E.T.S. de Ingenieros de Caminos, Canales y Puertos, Universidad de Castilla-La Mancha, 13071 Ciudad Real, (2008), 38:3, pp. 386-395.
15. Niloufar Zabihi, Effect of Specimen Size and Shape on Strength of Concrete, Submitted to the Institute of Graduate Studies and Research in Partial Fulfillment of the Requirements for the Degree of Master of Science in Civil Engineering, Eastern Mediterranean University, Gazimağusa, North Cyprus, (2012).
16. Farhad Aslani, Effects of specimen size and shape on compressive and tensile strengths of self-compacting concrete with or without

- fiber, Magazine of Concrete Research, ICE Publishing, (2013), 65:15, pp. 914-929
17. M.A.S. Sudin and M. Ramli, Effect of Specimen Shape and Size on the Compressive Strength of Foamed Concrete, published by EDP Sciences, MATEC Web of Conferences 10, 02003 published by EDP science, (2014).
 18. Raj Kumar, N. V. Mahure, Rajeev Gupta, P. K. Jha, S. L. Gupta and MurariRatnam, Establishing the correlation between compressive strength of small sized wet screened concrete cubes and full size large concrete cubes for mass concrete of dam, international journal of engineering sciences & management, Int. J. of Engg. Sci. & Mgmt. (IJESM), (2015), 5:2, pp. 26-31.
 19. RituKumari, Review Paper Based On the Relation between the Strength of Concrete Cubes and Cylinders, Int. Journal of Engineering Research and Applications www.ijera.com ISSN: 2248-9622, (2015), 5:8, (Part-2) pp.52-54.
 20. Misba Gul, Effect of Cube Size on the Compressive Strength of Concrete, IJEDR1604144 International Journal of Engineering Development and Research (www.ijedr.org) 956, (2016), 4:4 | ISSN: 2321-9939.
 21. Yi Che, Nan Zhang, Feng Yang and Mala Prafulla, Splitting tensile strength of self-consolidating concrete and its size effect, The 2016 world congress (structures 16), (2016), Jeju Island, Korea.
 22. PetarMatulić, Sandra Juradin, ElicaMarušić, Ante Domazet, Effect of test specimen size on mechanical properties of shotcrete. GRAĐEVINAR, (2016), 68:4, pp.301-309
 23. Gustavo Henrique Nalona, Roseli Oliveira GuedesMartinsa, Rita de Cássia Silva Sant'AnaAlvarengaa, Gustavo Emilio Soares de Limaa, Leonardo GonçalvesPedrotia, White José dos Santosb, Effect of Specimens' Shape and Size on the Determination of Compressive Strength and Deformability of Cement-lime Mortars, *Materials Research*, (2017), 20:2, pp. 819-825.
 24. Building Code Requirements for Structural Concrete (ACI318-14) and Commentary (ACI 318R-14), American Concrete Institute, P.O. Box 9094, Farmington Hills, Michigan.
 25. Ali Jihad Hamad, Size and shape effect of specimen on the compressive strength of HPLWFC reinforced with glass fiber, Journal of King Saud University-Engineering Sciences, (2017), 29, pp. 373-380
 26. Skazlic M. and Serdan M. and Bjegovic D., Influence of Test Specimens Geometry on Compressive Strength of Ultra High Performance Concrete, Second International Symposium on Ultra High Performance Concrete, Kassel, Germany, (2008), pp. 296-301.
 27. Al-Sahawneh, E.I., Size effect and strength correction factors for normal weight concrete specimens under uniaxial compression stress. *Contemp. Eng. Sci.*, (2013), 6:2pp.57-68.
 28. Kim, Jin.-keum., Seong-Tae, Y., Application of size effect to compressive strength of concrete members. *India*, (2002), 27:4, pp. 467-484.
 29. Malaikah, A.S., Effect of specimen size and shape on the compressive strength of high strength concrete. *Pertanika J. Sci. Technol.*, (2005), 13:1, pp. 87-96.

Source of Support: Nil
Conflict of Interest: None